



THE UNIVERSITY OF  
**TEXAS**  
— AT AUSTIN —

# Embodiment and Integrated Task and Motion Planning for Human-Centered Robots

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**The Human Centered Robotics Lab**

Aerospace Engineering

The University of Texas at Austin

Winter School, Toulouse, Dec. 5 2016

# Biogerontechnology and Assistive Technologies

(source: Fatronik 2007)

## Age      %disabled

60	13%
70	22%
80	42%
90	65%





Picture from Google search

## Human Centered Robotics:

The study of machines and robotic systems...

... with high mobility and sensing to assist, augment, or represent humans...

... in any way that will increase productivity, security, health and social comfort.

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About 323,000 results (0.56 seconds)

Scholarly articles for **human centered robotics**

**Human-centered robotics** applied to gait training and ... - **Riener** - Cited by 99

Intelligent space and **human centered robotics** - **Yamaguchi** - Cited by 67

**Human-centered robotics** and interactive haptic ... - **Khatib** - Cited by 60

The Human Centered Robotics Group – Decision and Control of ...

[sites.utexas.edu/hcrl/](https://sites.utexas.edu/hcrl/) ▾

21 Sep 2016 - We are very pleased to have an all star line up of keynote speakers for the IEEE International Workshop of Advanced **Robotics** and its Social ...

People · Publications · Research · Courses

**Human-Centered Robotics Lab - University of Washington**

<https://hcrlab.cs.washington.edu/> ▾

**Human-Centered Robotics** Lab Computer Science & Engineering Department | University of Washington. ; ,. Faculty. Graduate Students. Visitors ...

**Brown University Humanity Centered Robotics Initiative – The next ...**

<https://hcri.brown.edu/> ▾

"Malle suspects that we might actually want our **robots** to make different decisions than the ones we'd want other **humans** to make . . .[in a life or death scenario] ...

## Human Factors in Space Station Architecture II

*EVA Access Facility: A Comparative  
Analysis of Four Concepts for  
On-Orbit Space Suit Servicing*

Marc M. Cohen  
*Ames Research Center*

the Skylab mission (ref. 2).

Since 1982, the Space Transportation System (STS) places increasing emphasis upon the regular use of EVA for in-flight development, recovery, and repair of space systems. This trend is expected to continue on the Space Station. The dexterity of the human operator in EVA is transmitted through the human/machine interface imposed by the protective envelope of the suit; hence, significant advances in EVA capability are due primarily to improvements in the design of the space suit. The primary goal of space suit design is to reduce losses in human dexterity and in mobility to the

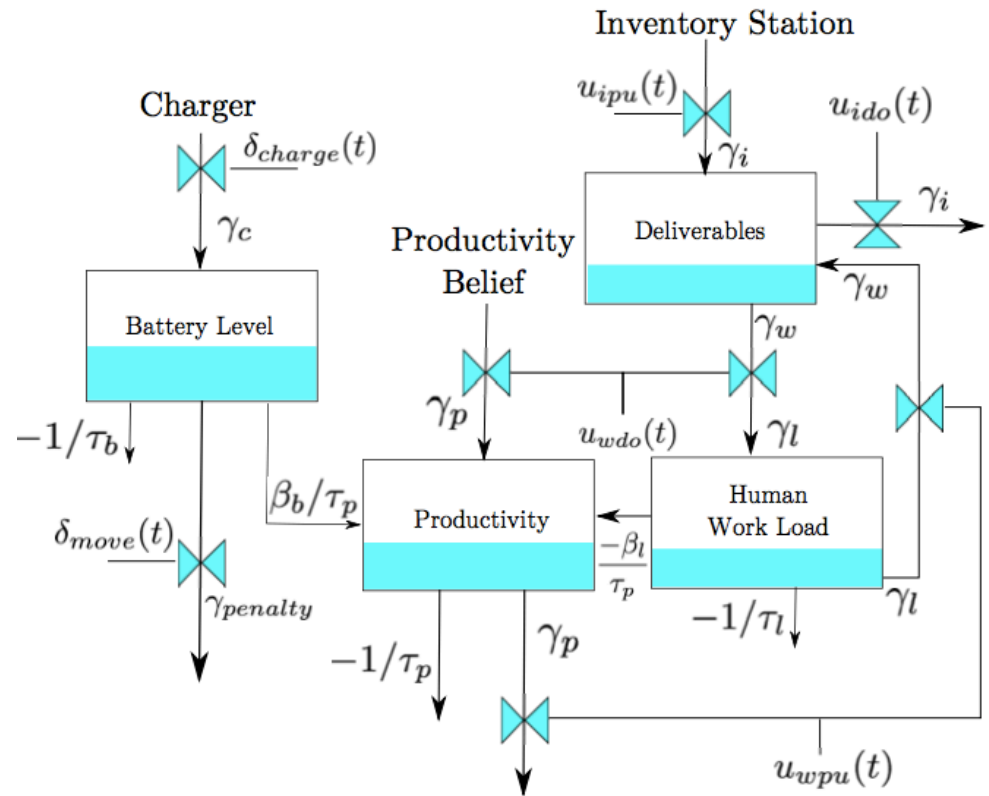
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\*Massachusetts Institute of Technology, Cambridge, MA.

Disney Co.



The University of Texas at Austin



### References:

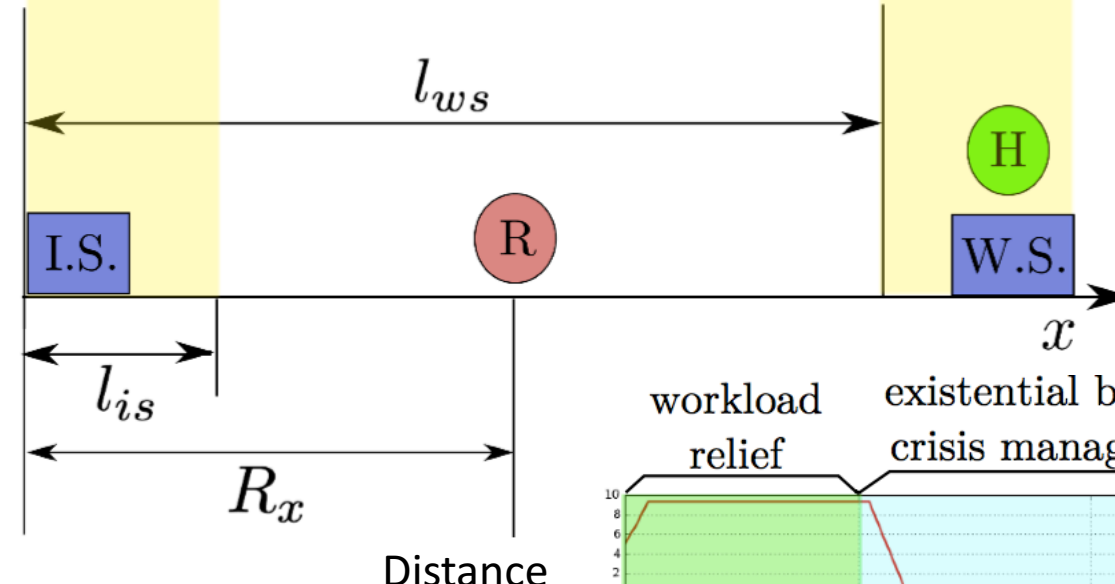
W. T. Riley, D. E. Rivera, A. A. Autienza, W. Nilsen, S. Allison, and R. Mermelstein, Health behavior models in the age of mobile interventions: are our theories up to the task? *Translational Behavioral Medicine: Practice*, 2011

A. Martin, D. E. Rivera, W. T. Riley, E. B. Hekler, M. P. Buman, M. A. Adams, and A. C. King. A Dynamical Systems Model of Social Cognitive Theory, *American Control Conference*, 2014.

# HRI-Scenario I

Inventory Station Area

Human Work Station Area



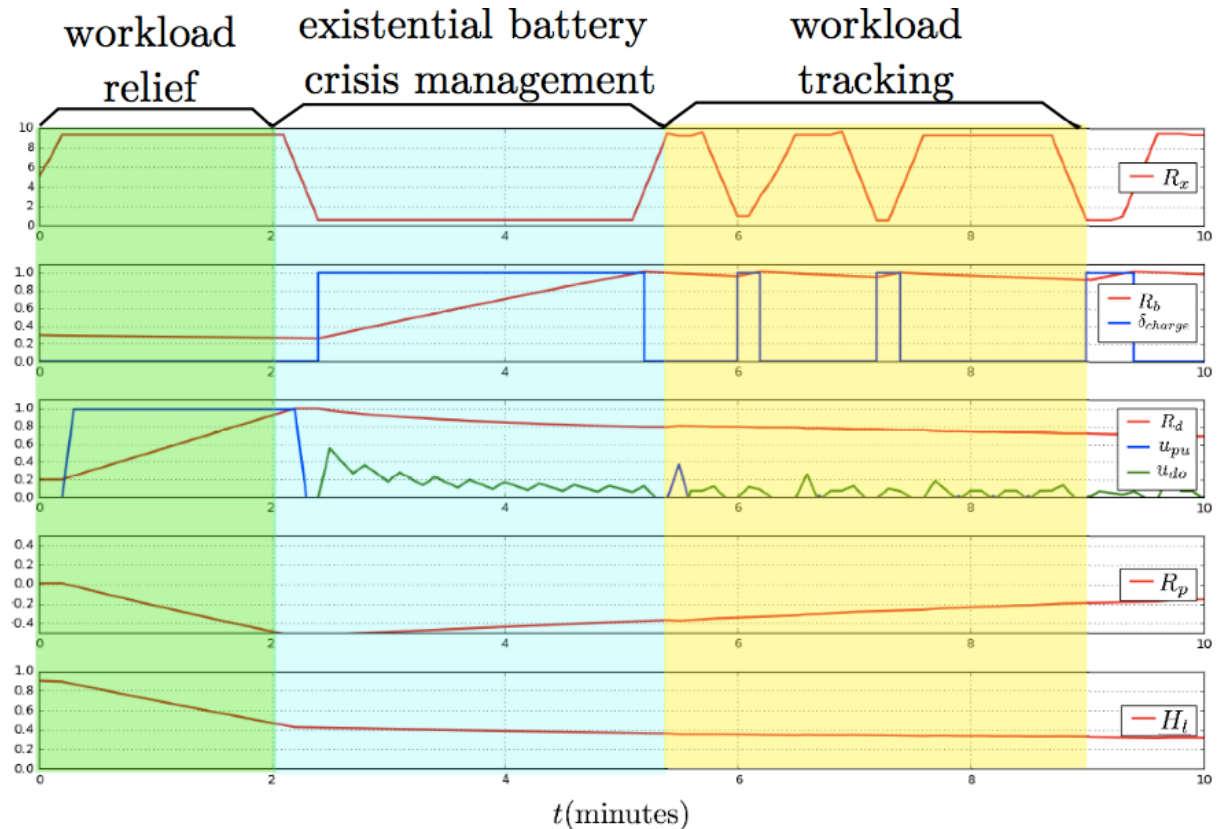
Distance

Battery level

Amount of deliverables

“Robot” productivity

Human workload



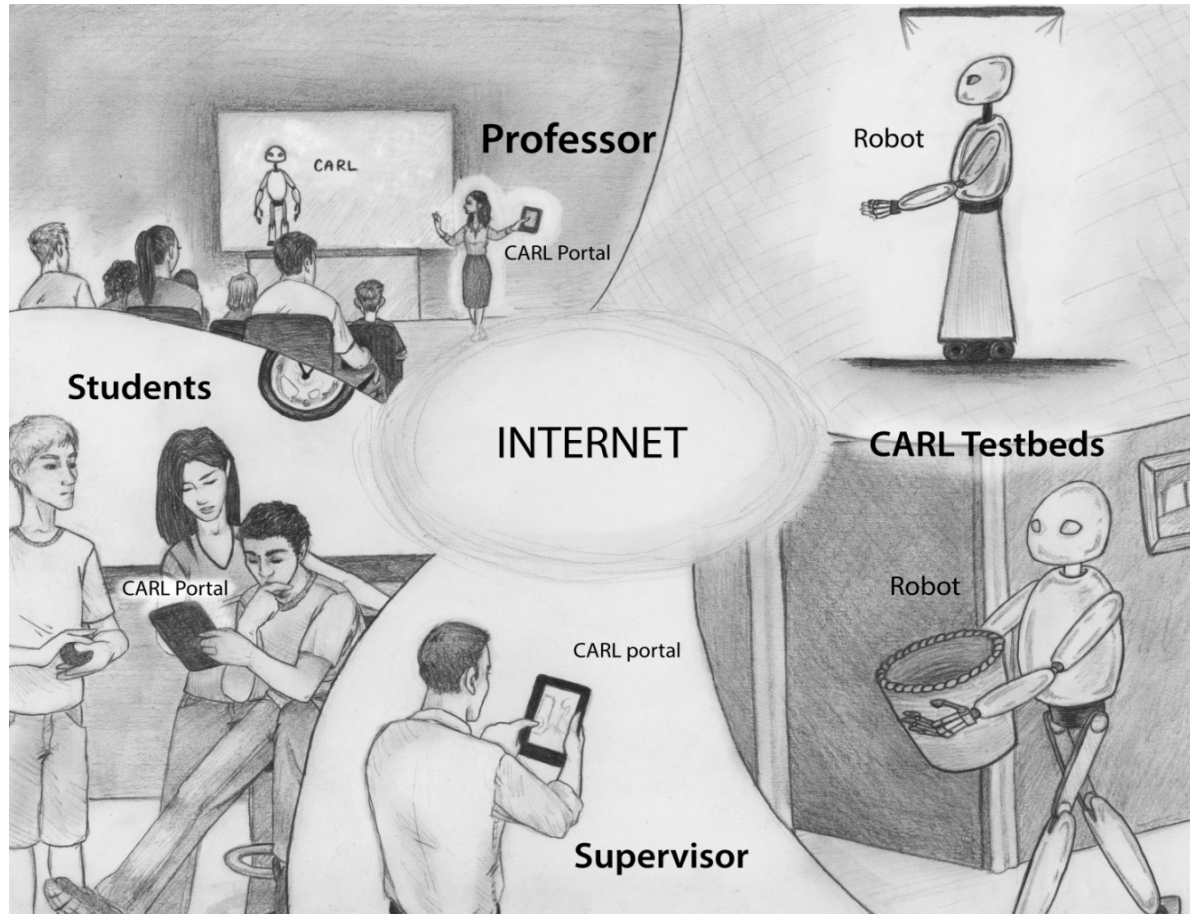
(b) 30% Robot battery & 90% human workload at  $t=0$

Dreamer means: No, I don't know you

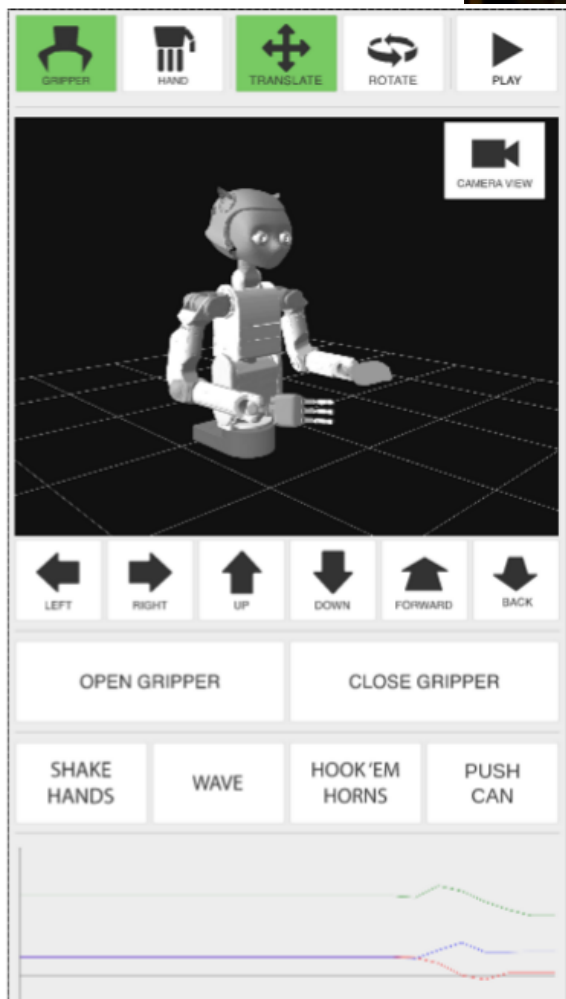




# 2014 Concept on Shared Equipment



C.L. Fok, F. Sun, M. Mangum, A. Mok, B. He, L. Sentis, Web Based Teleoperation of a Humanoid Robot, arXiv:1607.05402 [cs.RO]



Devices  
Democratizing ~~Robots~~ via  
Smart and Shared  
Educational Content

# Snapshots

**Mara Altman**

Shared Laboratory Initiative

October 24th - 28th, 2016

	MON	TUES	WED	THU	FRI
08:00	OPEN	OPEN	OPEN	OPEN	OPEN
09:00	OPEN	OPEN	OPEN	OPEN	OPEN
10:00	OPEN	OPEN	OPEN	OPEN	OPEN
11:00	OPEN	OPEN	OPEN	OPEN	OPEN
12:00	OPEN	OPEN	OPEN	OPEN	OPEN
13:00	OPEN	OPEN	OPEN	OPEN	OPEN
14:00	OPEN	OPEN	OPEN	OPEN	OPEN
15:00	OPEN	OPEN	OPEN	OPEN	OPEN
16:00	OPEN	OPEN	OPEN	OPEN	OPEN
17:00	OPEN	OPEN	OPEN	OPEN	OPEN
18:00	OPEN	OPEN	OPEN	OPEN	OPEN

Experiment 1 Completed

Experiment 2 Completed

Experiment 3 Completed

Add experiment

Schedule

**Matt Mangum**

Shared Laboratory Initiative

Experiment 1 Completed

Experiment 2 Completed

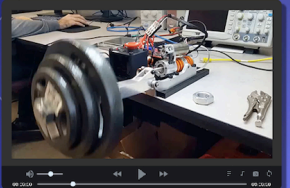
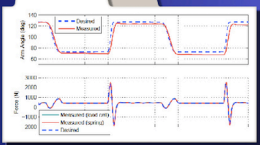
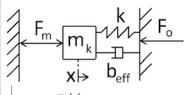
Experiment 3 Completed

Add experiment

Pre-lab Activities

Lab Activities

Post-lab Activities

$$P(s) = \frac{F_o(s)}{x(s)} = \frac{Nk_s \eta k}{s^2}$$

$$P(s) = \frac{F_o(s)}{x(s)} = \frac{Nk_s \eta k}{m_2 s^2 + b_{eff} s + k}$$

$$P(s) = \frac{F_o(s)}{x(s)} = \frac{Nk_s \eta k}{b_{eff} s + k}$$

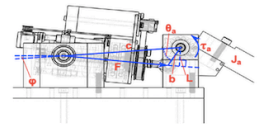
Submit

**Matt Mangum**

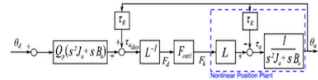
Shared Laboratory Initiative

### Prelab

The previous three experiments give us a force controller with disturbance observer, which takes in desired force  $F_d$  and outputs spring force  $F_k$ . Now we will build a position controller upon the force controller. Figure 1 shows the geometry of a revolute joint the actuator attaches.  $L$  is linkage moment arm,  $c$  is distance between the actuator pivot and the arm pivot,  $b$  is distance between the arm pivot and the pushrod pivot.  $F$  is actuator force.  $\theta$  is torque exerted on the output arm.  $J_a$  is inertia of the output arm.  $\phi$  is offset angle.



Now we consider the SEA with force controller as a single block in the block diagram Fcntrl. We will use feedforward control to build our position controller this time. Figure 2 shows the block diagram of the position controller that we will build later.  $\tau_{ag}$  is gravity compensation torque.  $L$  is nonlinear linkage kinematics.  $Q_p$  is a low-pass filter.



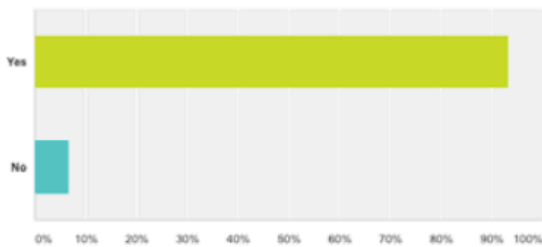
The blocks in the dashed blue region belong to the plant of the revolute joint, which takes the spring force  $F_k$  and outputs joint position  $a$ . Based on Figure 1, we can find out the relationship inside this plant box:

$$\tau_a = J_a \ddot{\theta}_a + B_a \dot{\theta}_a + \tau_g(\theta_a) = F_k L(\theta_a)$$

# Surveys + Information eXperience

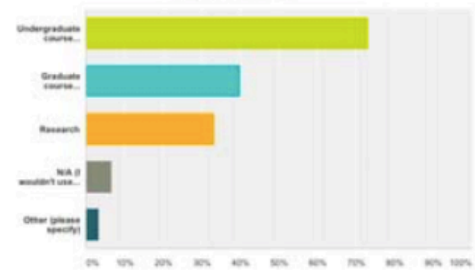
Would you consider using, at least once, such a platform for educational or research purposes?

Answered: 30 Skipped: 0



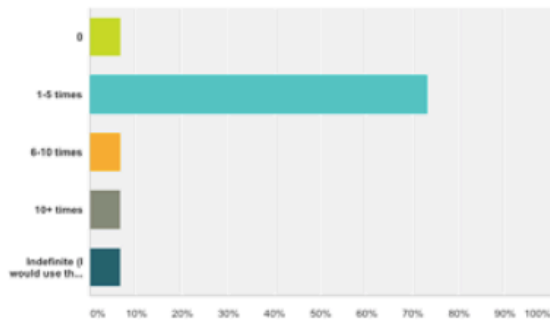
How would you use this type of system (Select all that apply)

Answered: 29 Skipped: 0



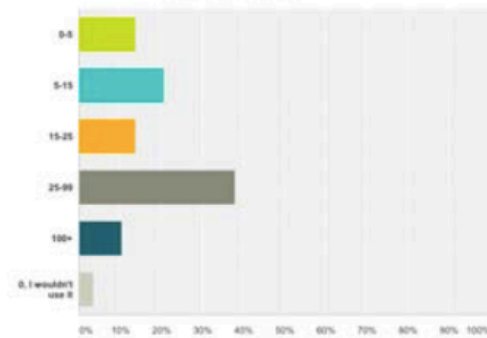
How many times during a semester would you consider using this platform?

Answered: 30 Skipped: 0

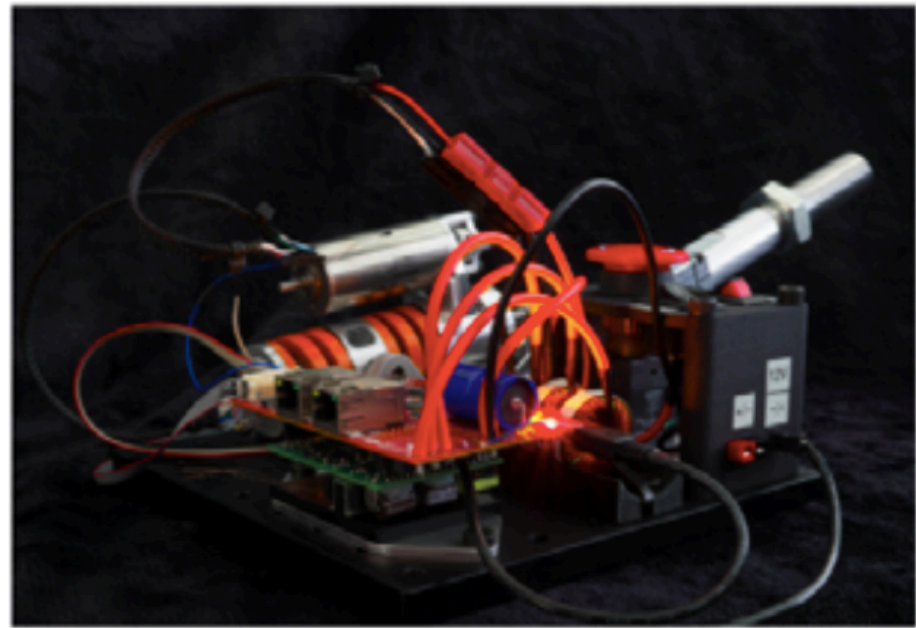
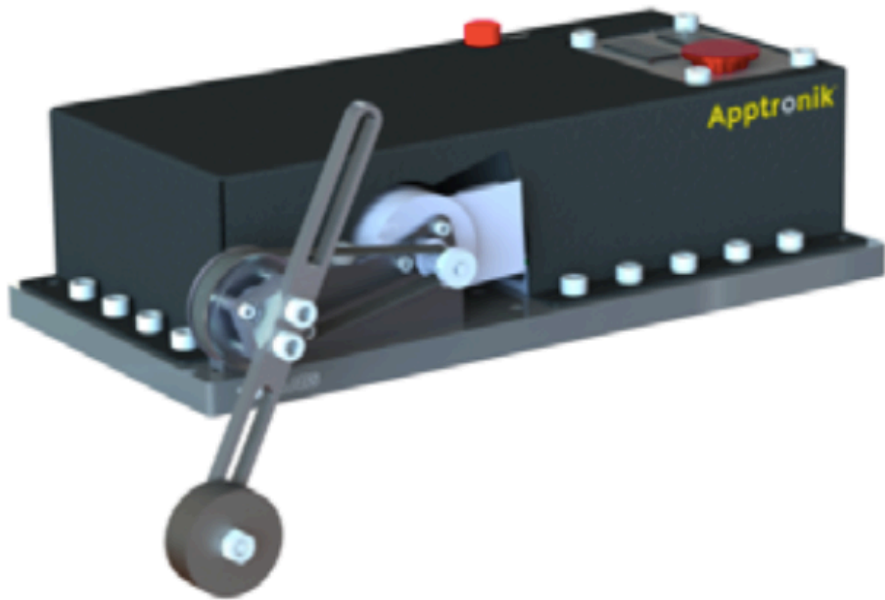


How many users would utilize this system?

Answered: 29 Skipped: 1



# Apptronik's role



# Course Decision and Control of Human-Centered Robots

WEEK	TOPIC
Th 8/25	Syllabus / Background / Introductions / Project Teaming
Week 8/30	Intro Autonomous Systems, Socio Cognitive Modeling of Human Activity
Week 9/6	Unconstrained and constrained optimization, 1st and 2nd Order Solvers, Lagrangian Multipliers, Optimal Control, Model Predictive Control (MPC)
Week 9/13	Socio-Cognitive Behavior Intervention via MPC, Mixed Integer Programming
Week 9/20	Case Study: Behavior Interventions on Exercising Activity
Week 9/27	Introduction to Sequential Composition, LQR-Trees Theory
Week 10/4	LQR-based Linearization along Trajectories, Regions of Attraction via SOS Tools, Case Study: Nonlinear Underactuated System Stabilization
Week 10/11	Intro to Motion Planning with LTL Specifications, Lifted Graphs, Admissible Paths, Intro to Linear Temporal Logic
Week 10/18	Transition Systems Incorporating Geometric and Temporal States, Mission Compliant Paths, Intro Automata Theory
Week 10/25	Nonlinear Controller Synthesis and Automatic Workspace Partitioning for Reactive High-Level Behaviors
Week 11/1	Intelligent Collision Management in Human-Centered Robots
Week 11/8	Provably Safe Obstacle Avoidance for Autonomous Robotic Ground Vehicles
Week 11/15	Stabilizing Series-Elastic Point-Foot Bipedes Using Whole-Body Operational Space Control, Integrated Task and Motion Planning
Week 11/22	Details ONR MURI Autonomous Systems, Thanksgiving Holiday
Week 11/29	<b>Final Project Presentations</b>

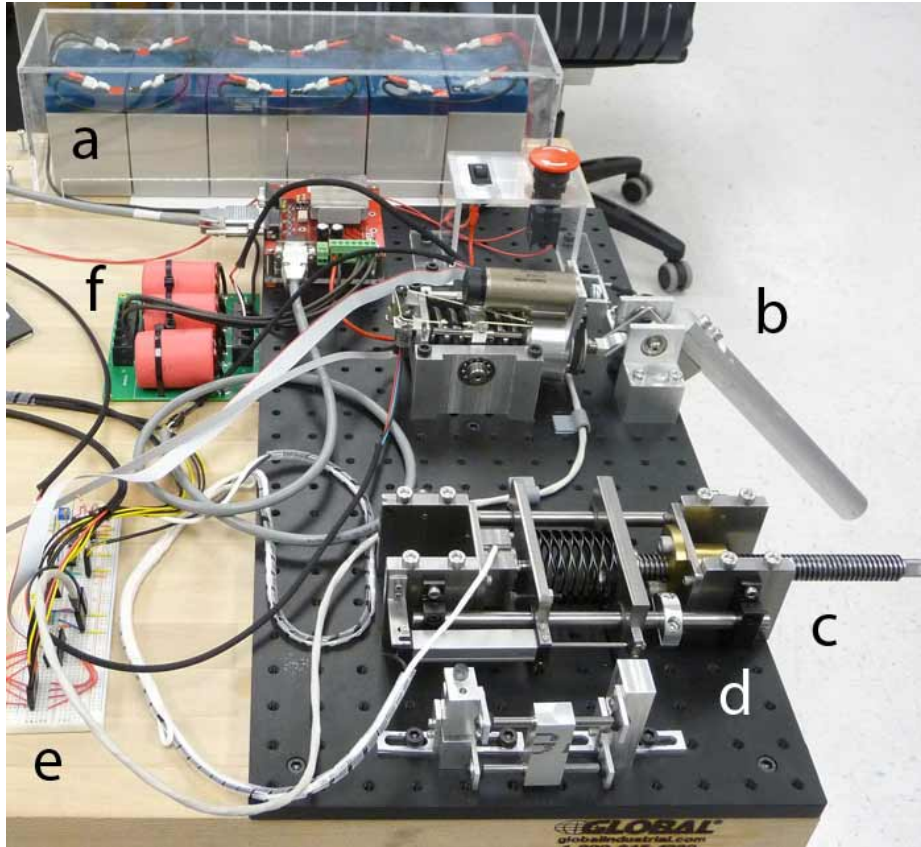
# Let's change topic...

## Embodiment

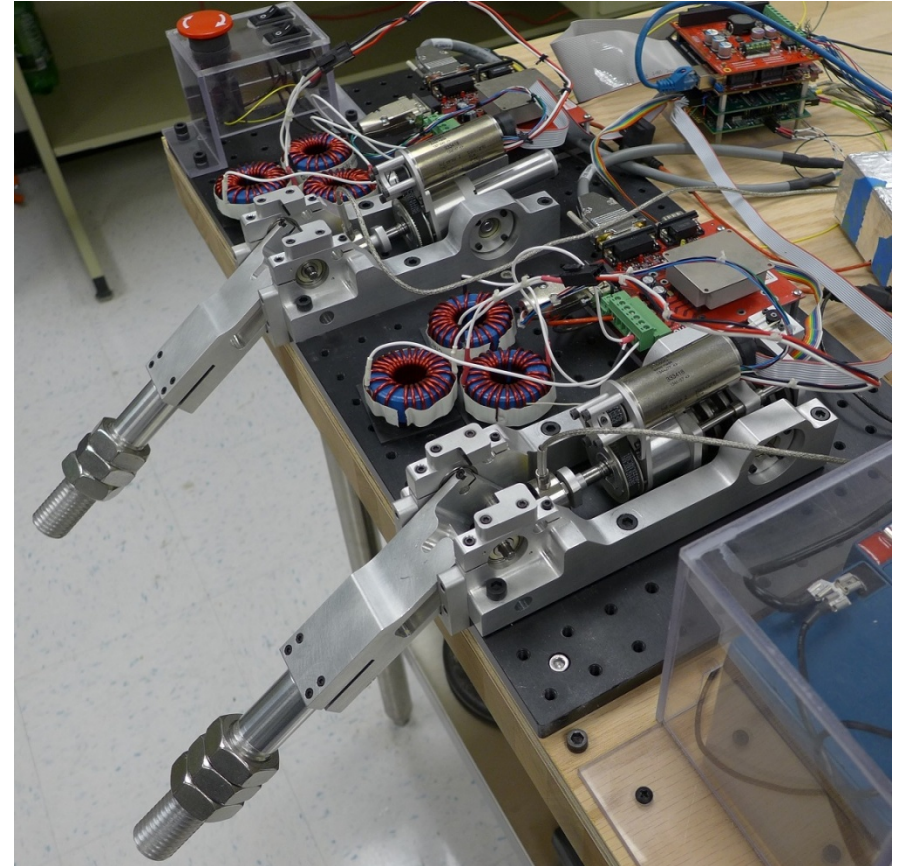


# UT Testbeds

Original UT-SEA testbed



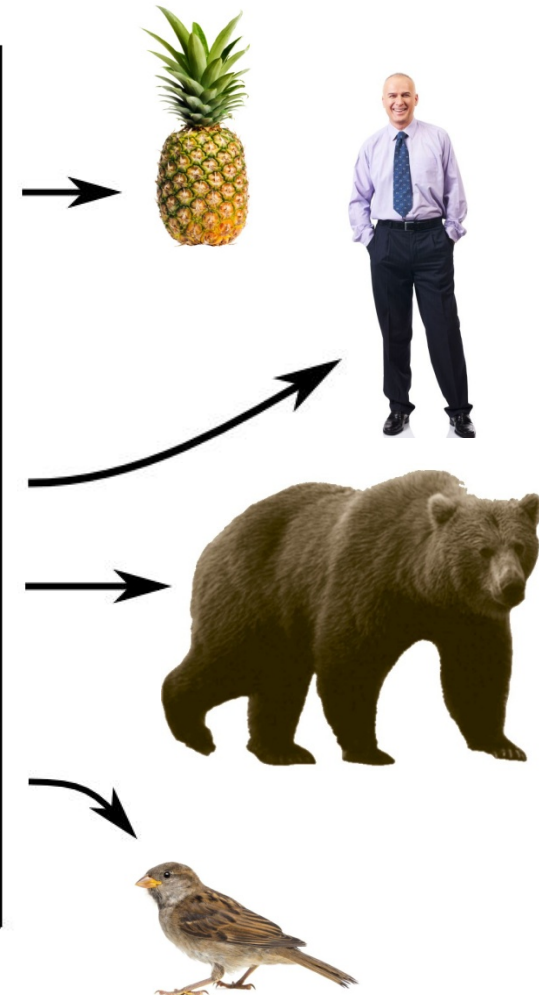
UT-SEA Version 2 testbed





# Specifications

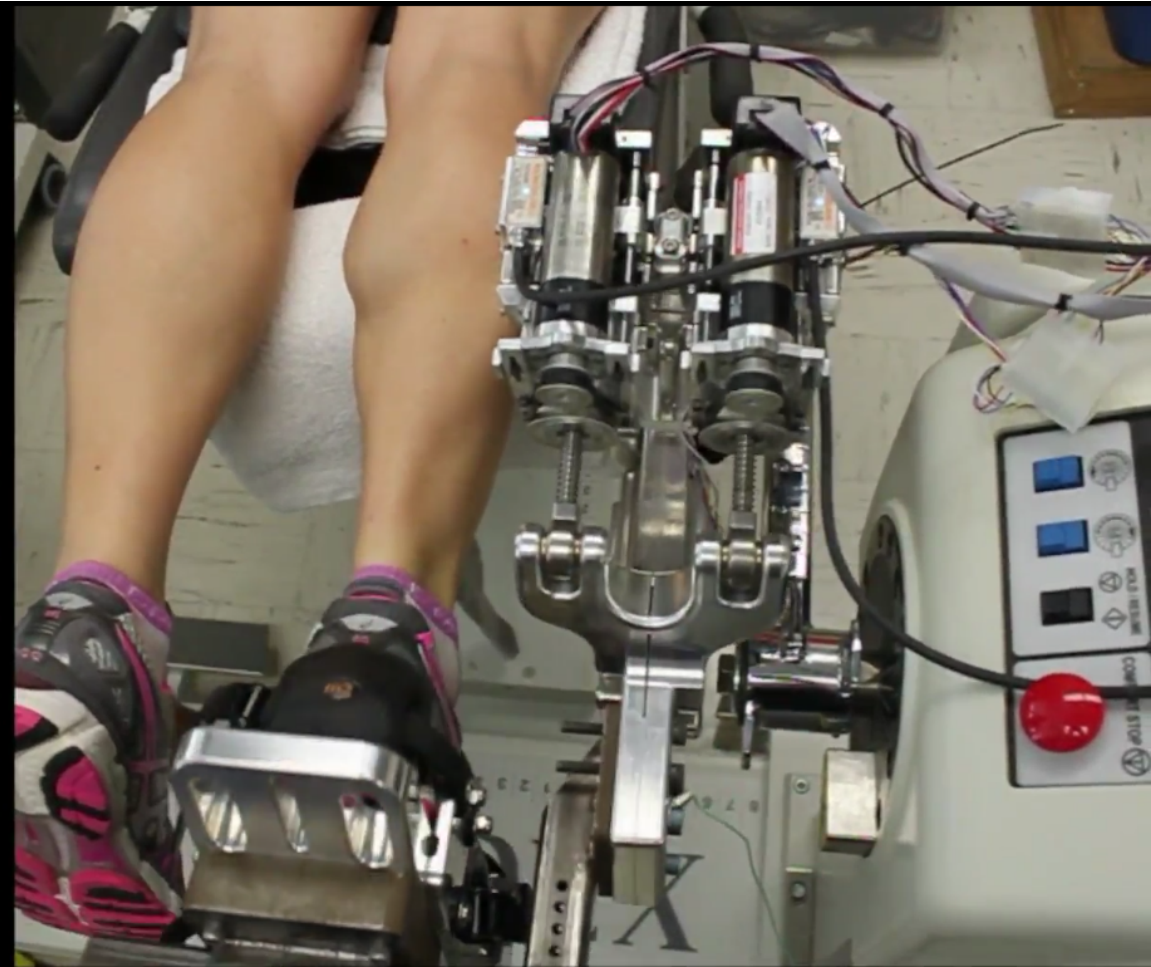
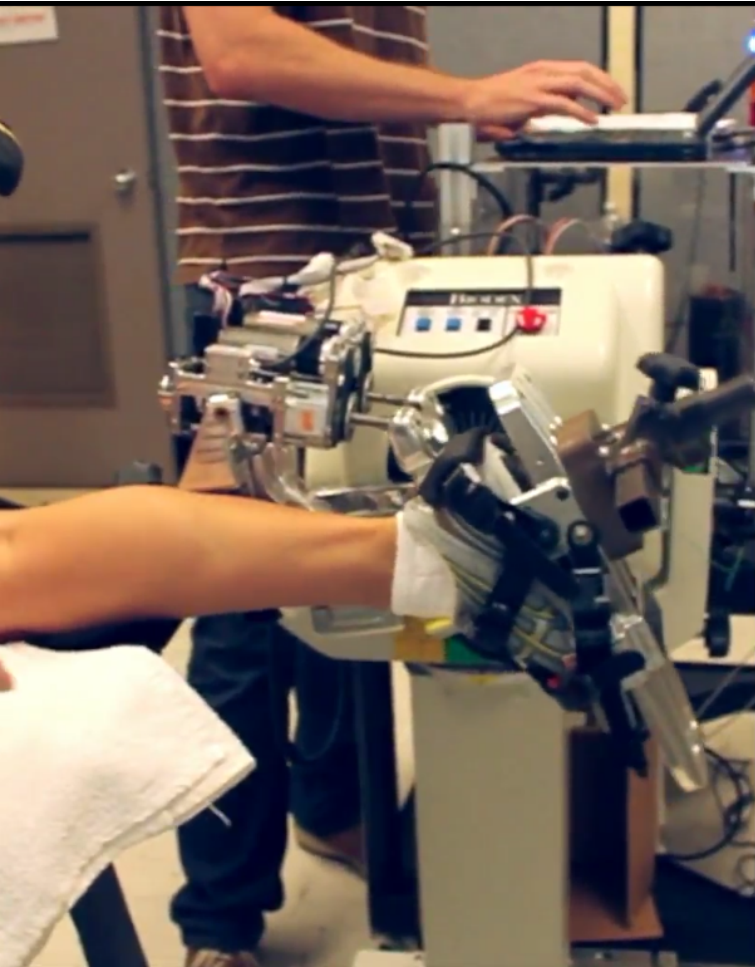
UT-SEA Design Specifications		
Weight	1013 g	2.23 lbs
Stroke	6 cm	2.36 in
Max Speed	32.5 cm/sec	12.79 in/sec
Continuous Force	848 N	190 lbs
Intermittent Force	2800 N	629 lbs
Spring Stiffness	278 N/mm	1587 lbs/in
Force Resolution	0.31 N	0.069 lbs
Operating Voltage	80V	



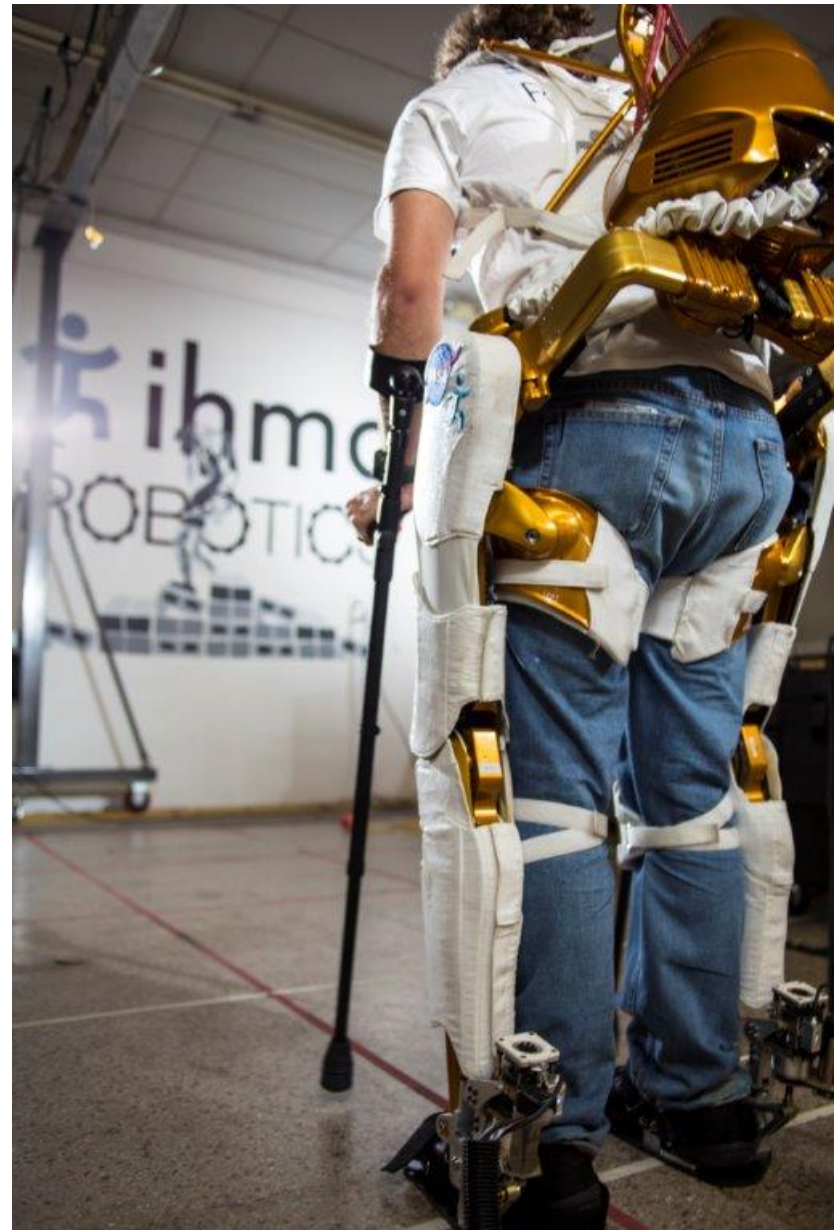
# 2013 adoption

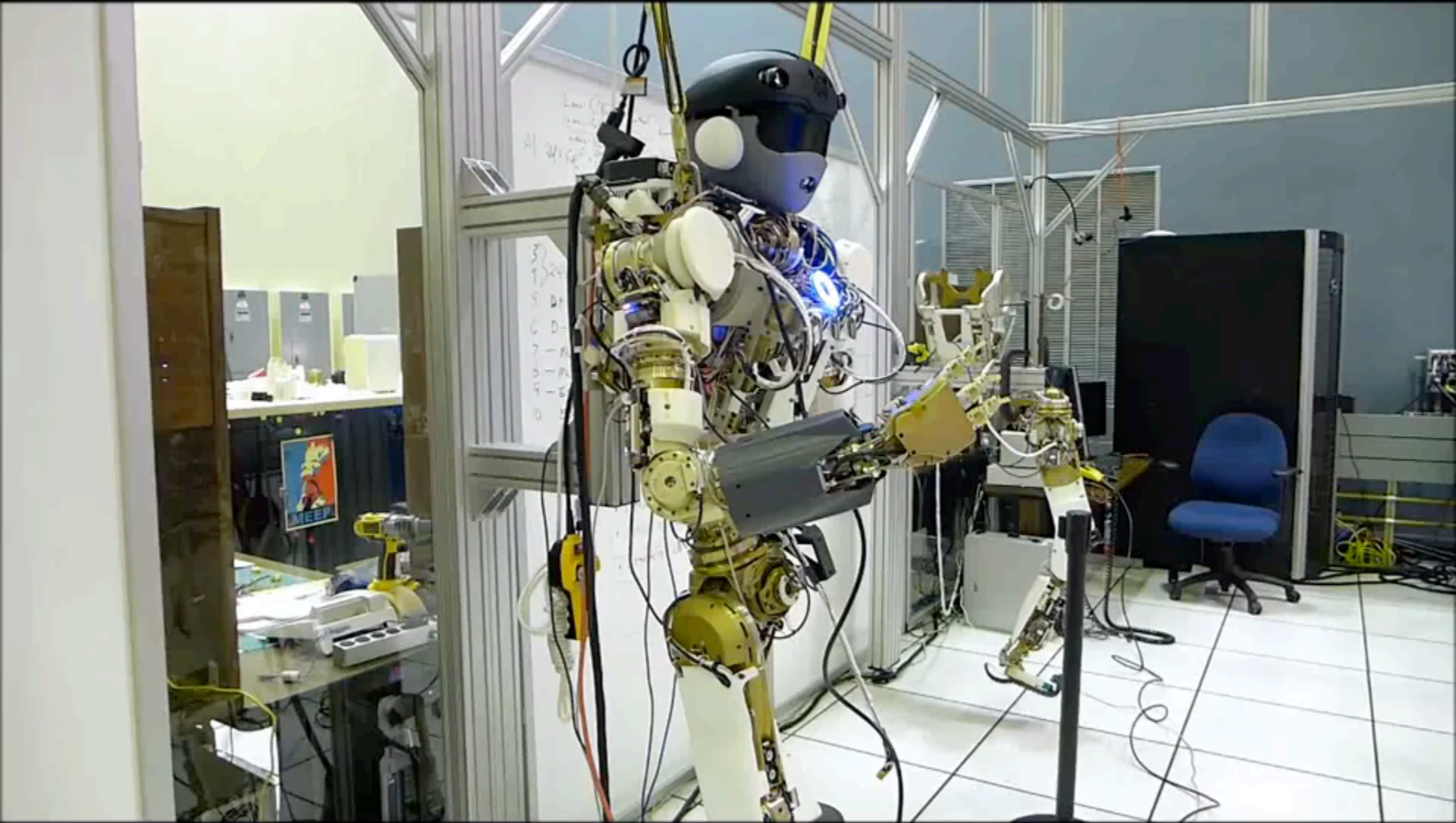


# Rehabilitation Systems



# X1 Mina Exo

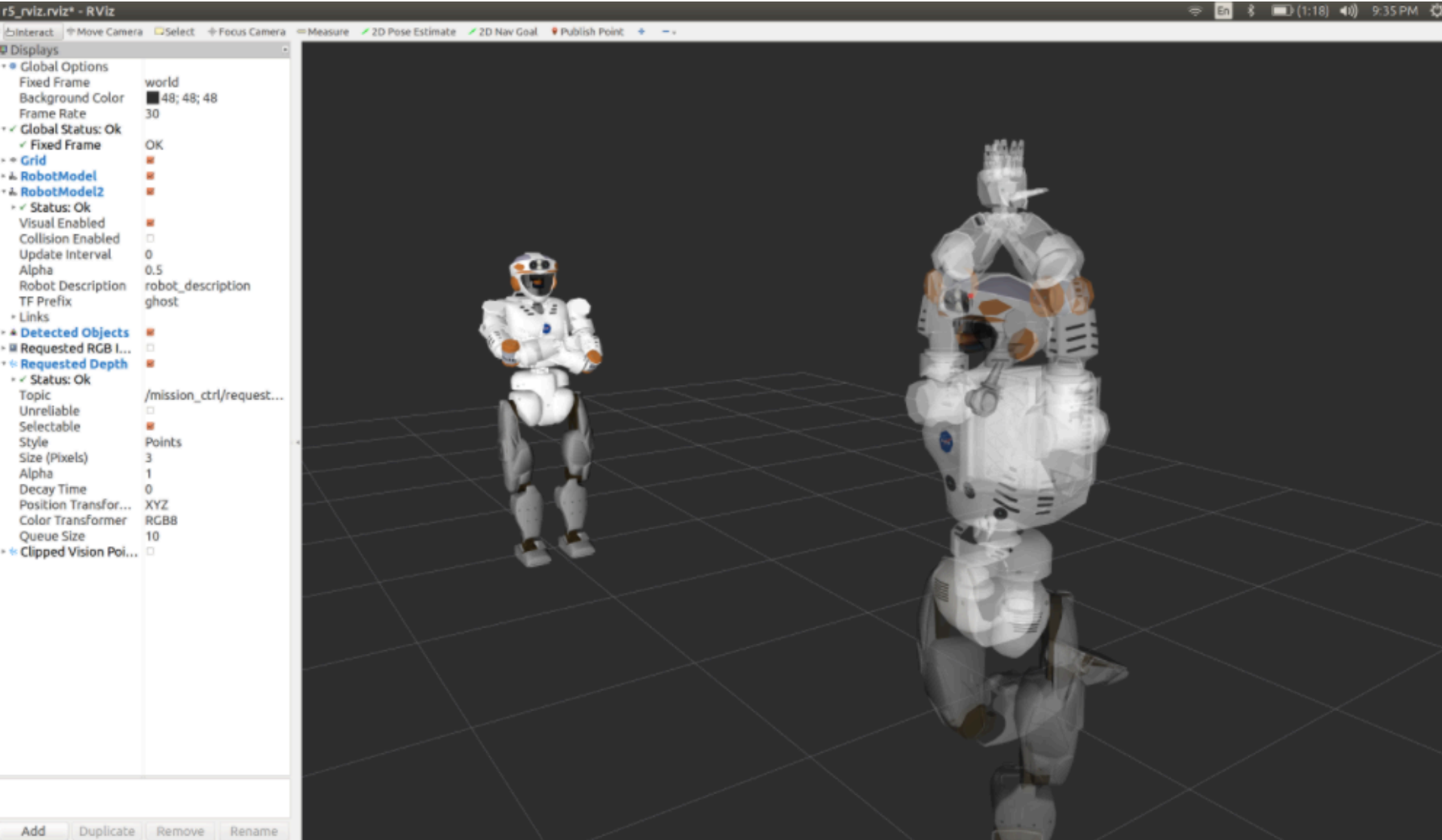




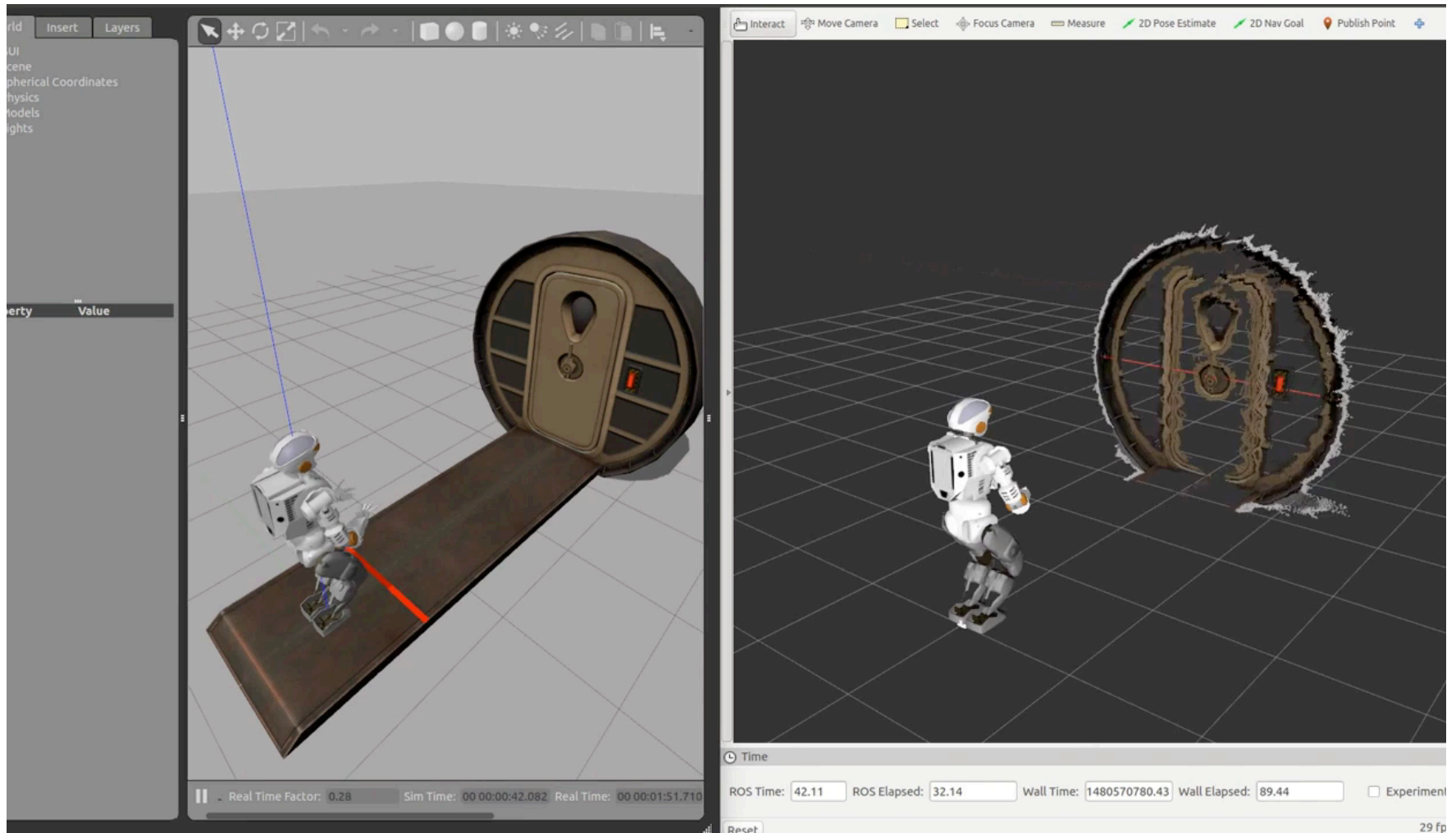
# Valkyrie Program



# So, what are we doing today ;)

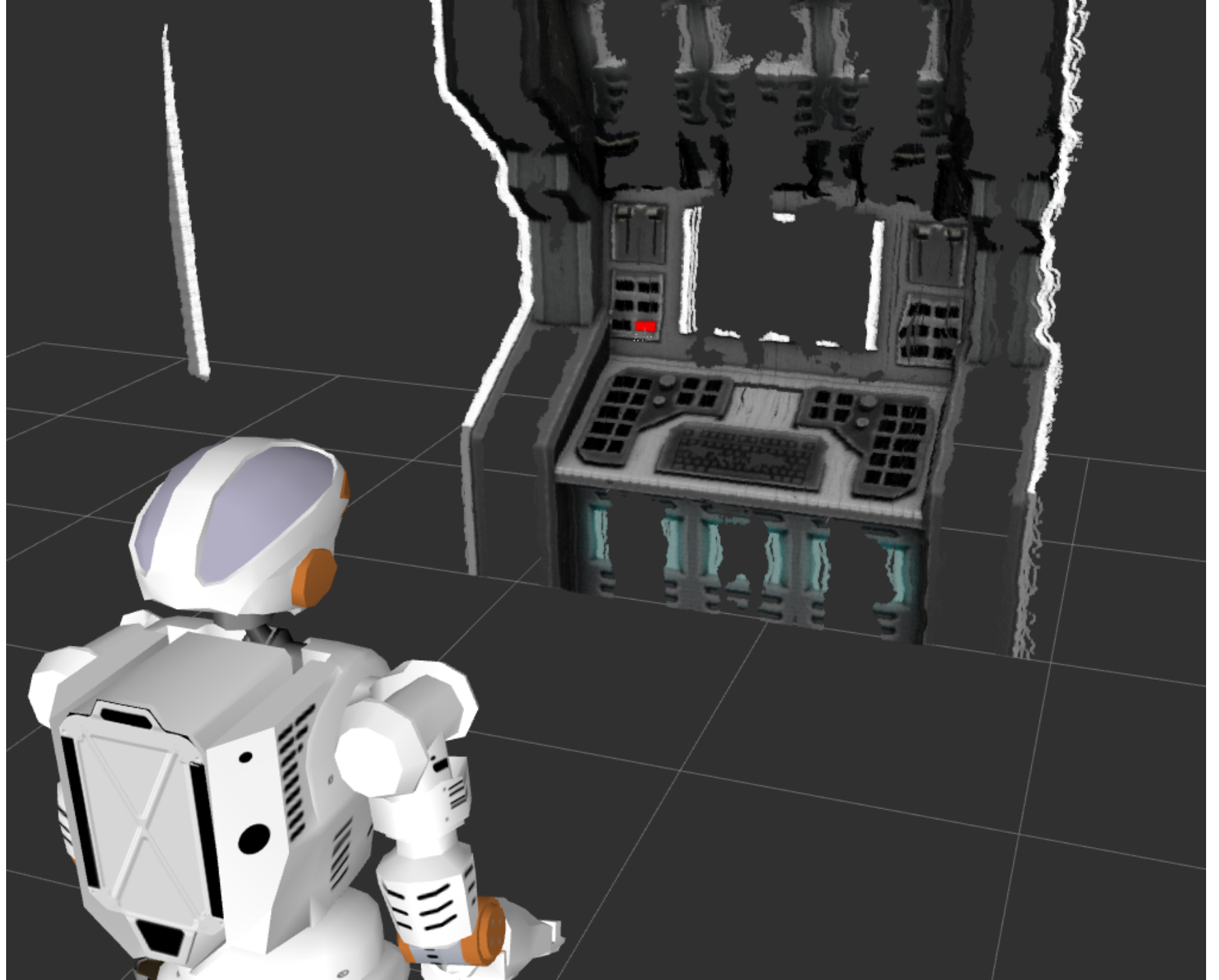


# NASA Space Robotics Challenge



Mission 2 SRC: The Human Centered Robotics Lab + various UT Austin Students







REVENUE

R&D

Product Development and Sales

Robotic Engineering Solutions Center

Humanoid Robot Program

**Hardware**

**Service Model**

- Actuators
- Axon Control Circuits
- Liquid Cooling System

Provide robotic engineering design solutions to industry and government.

- Hardware Solutions
- Software Solutions

**Software**

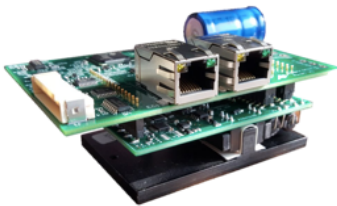
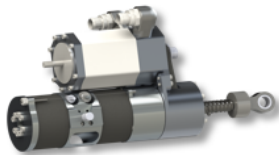
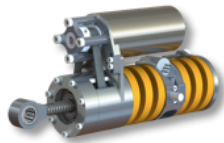
- Human Touch Sensing
- Centralized Actuator Control Software
- Whole Body Control

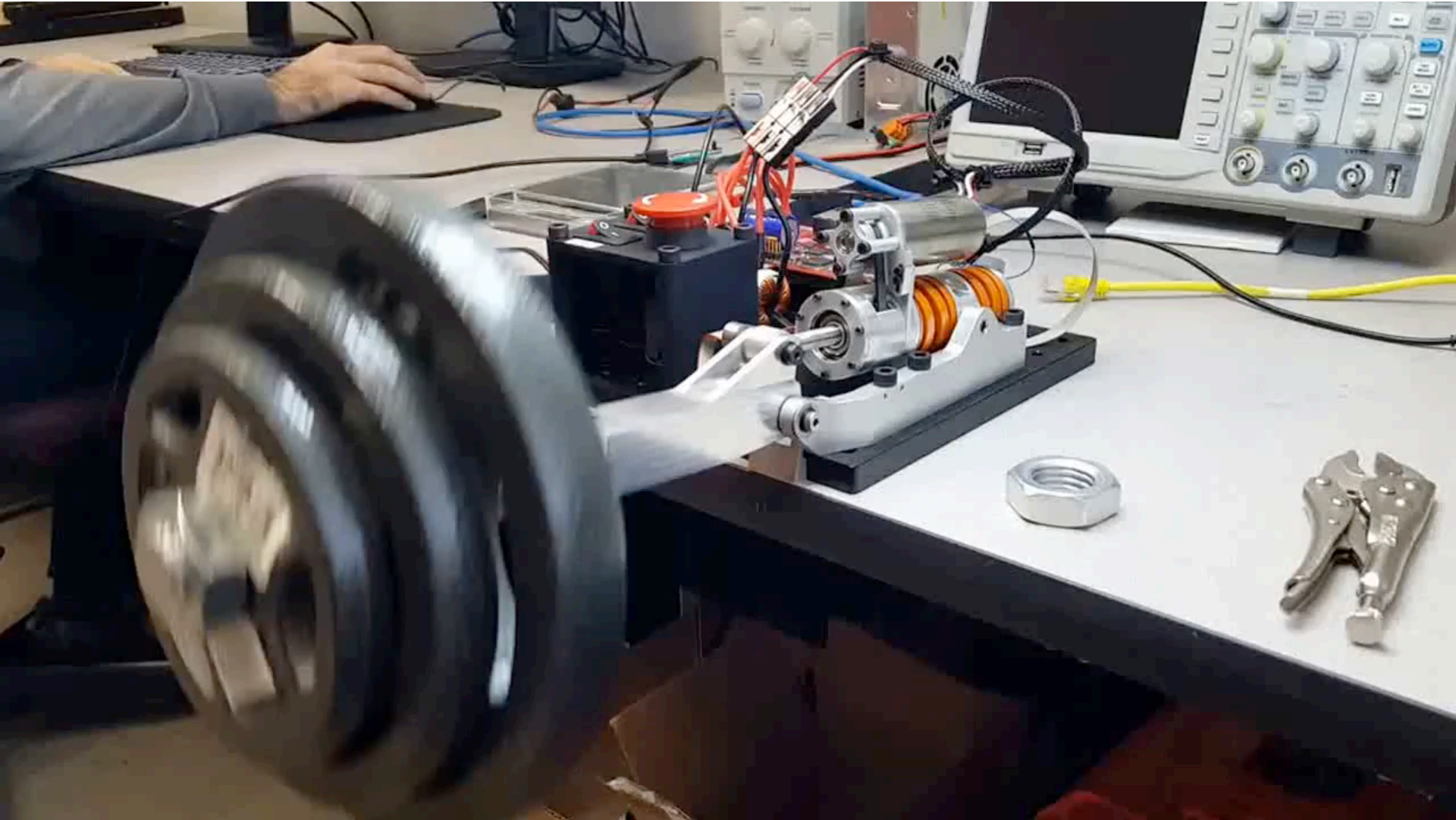
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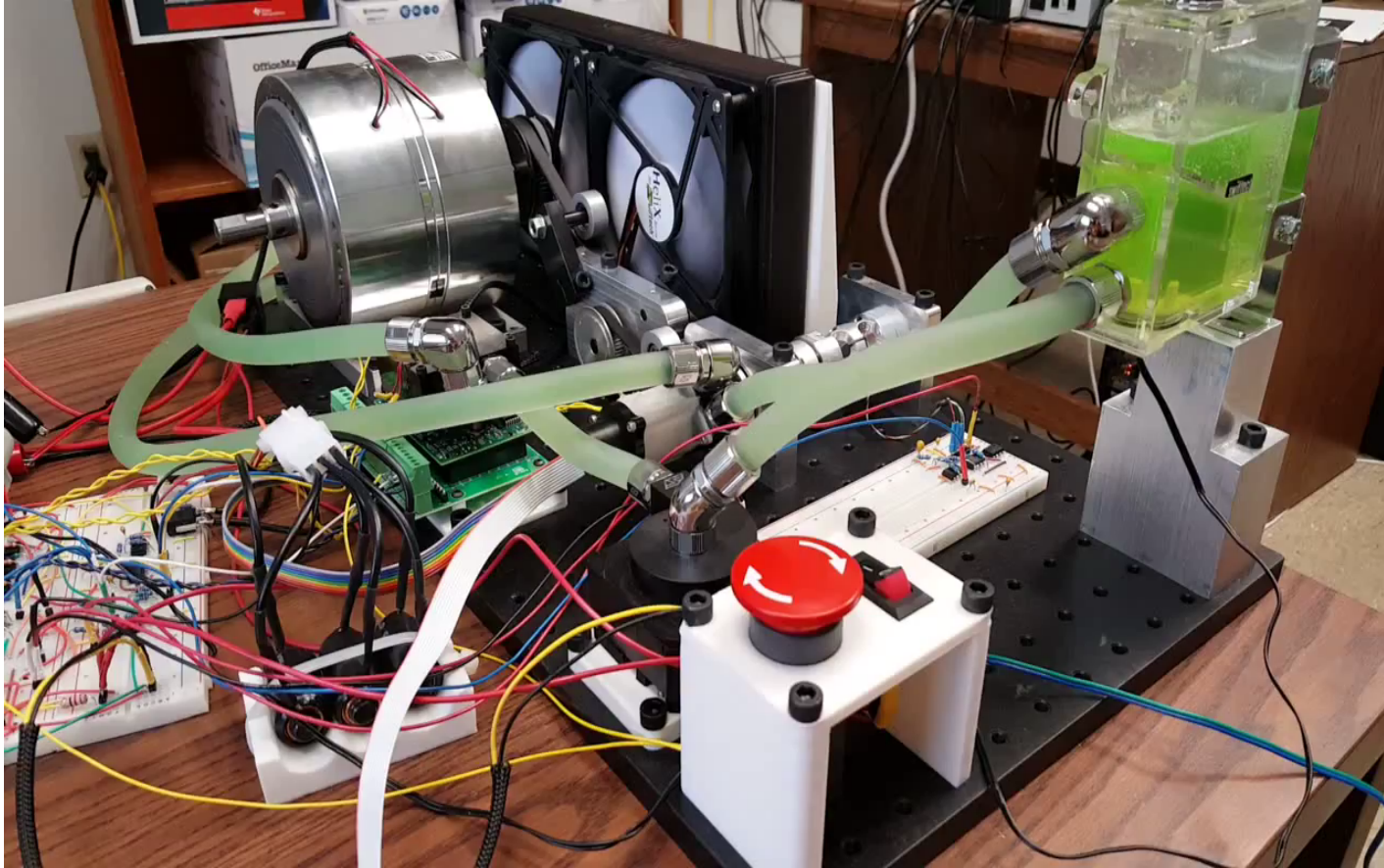
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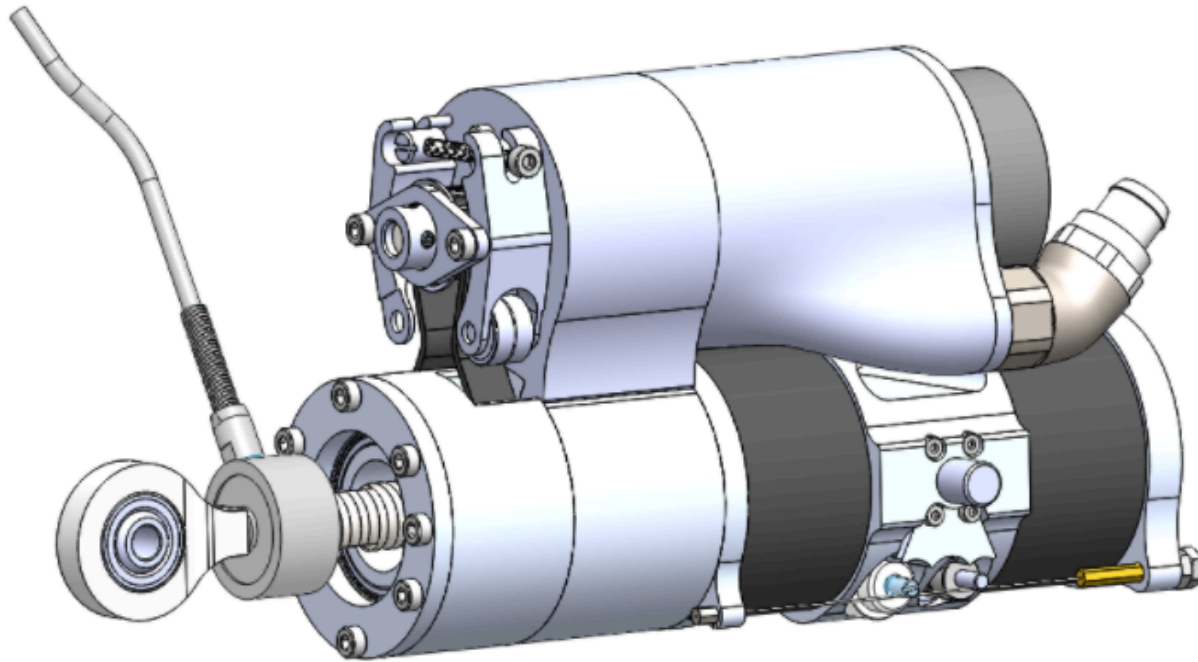
**Objective:**  
Design and build a humanoid robot





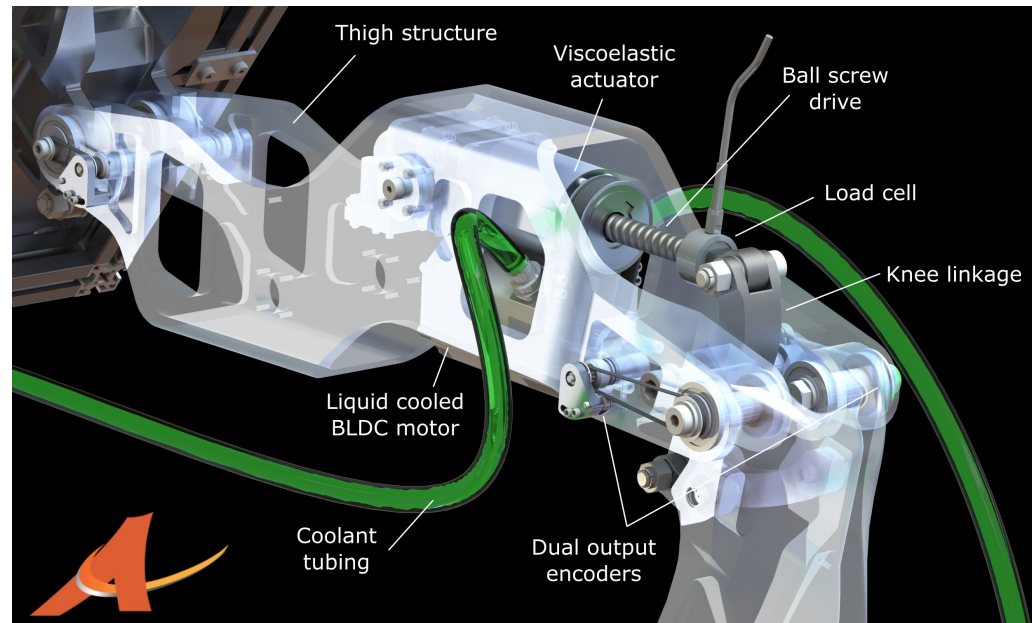
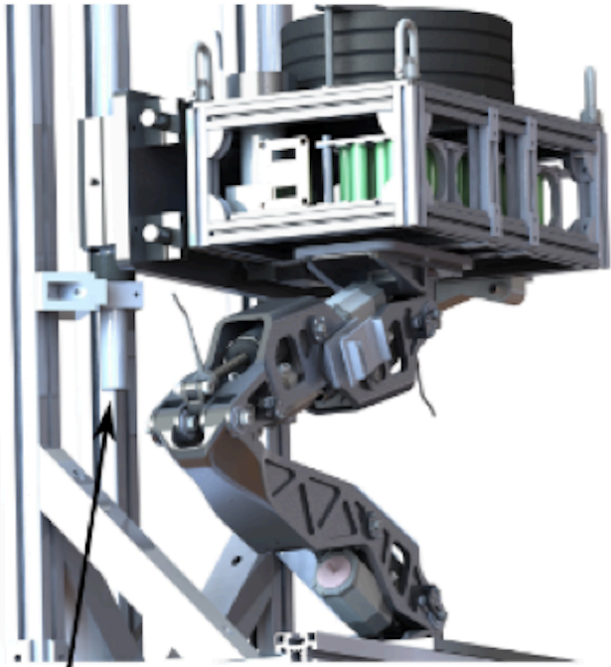
# Building systems for agility





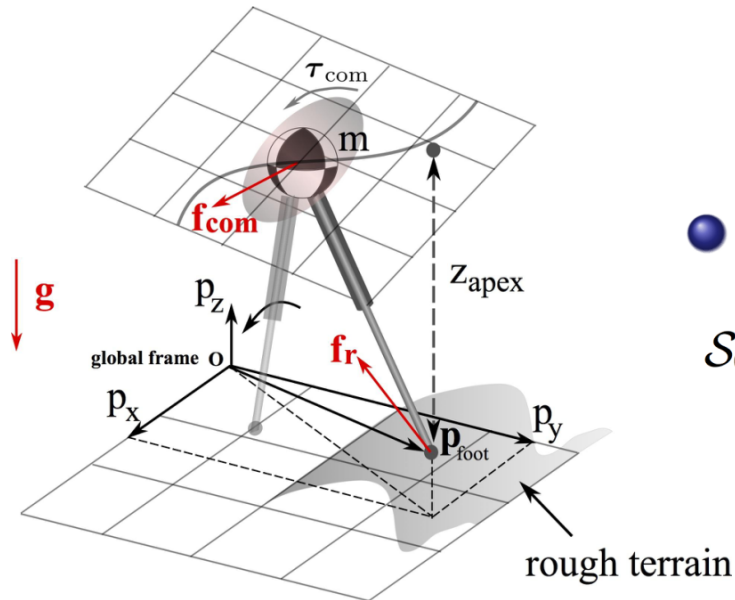
Liquid Cooled  
Viscoelastic Actuator

# More to come



# Agility is Key Interest...

## Dynamic Locomotion



- Center of mass surface manifold

$$\mathcal{S}_{\text{CoM}} = \left\{ (x, y, z) \in \mathbb{R}^3 \mid \psi_{\text{CoM}}(x, y, z) = 0 \right\}$$

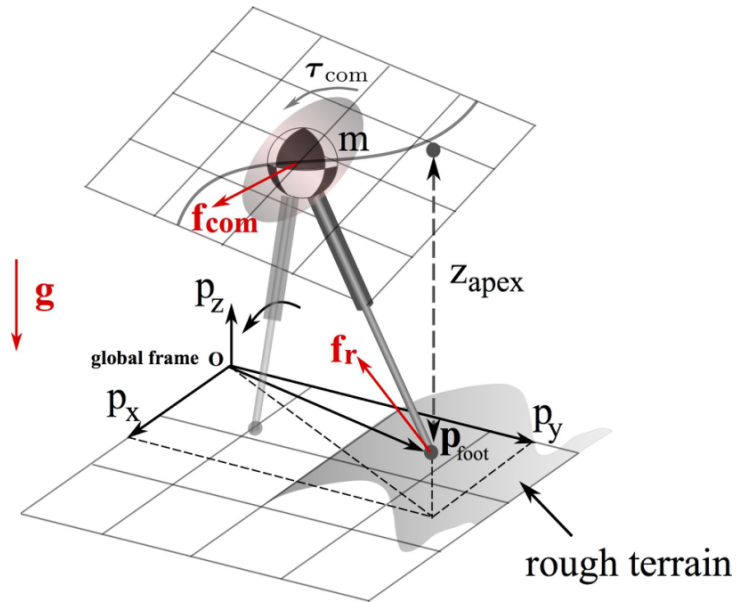
### Output Dynamics of the Center of Mass

The prismatic inverted pendulum model for a  $q^{\text{th}}$  walking step, is represented by the following control system,

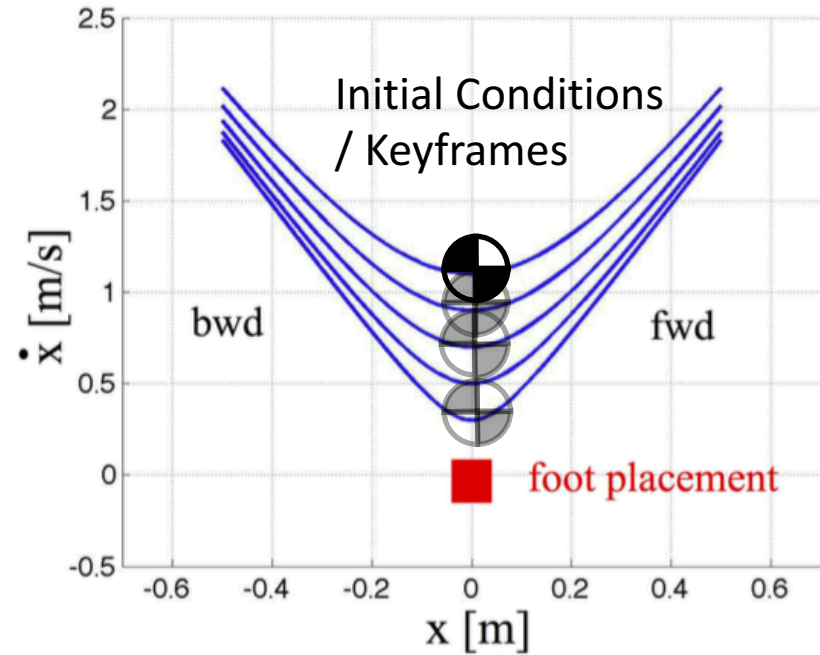
$$\dot{\xi} = \mathcal{F}(q, \xi, u) \quad (\text{PIPM dynamics})$$

where  $\xi = (x, y, z, \dot{x}, \dot{y}, \dot{z})^T$ ,  $u = (\omega, \tau, \mathbf{p}_{\text{foot}})^T$ .

# Keyframe states

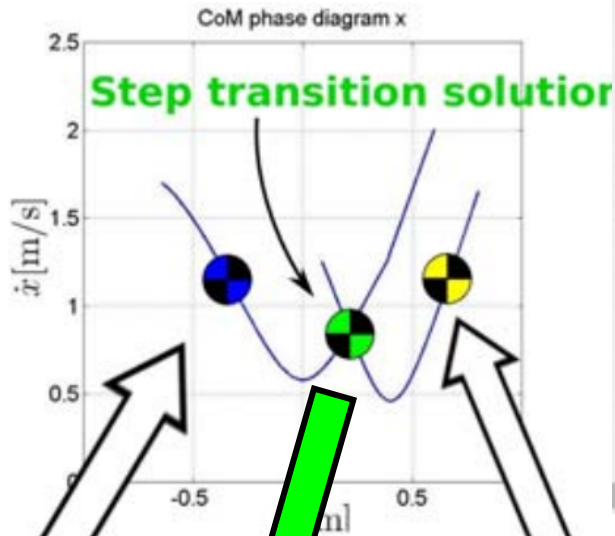


Phase Portrait Center of Mass



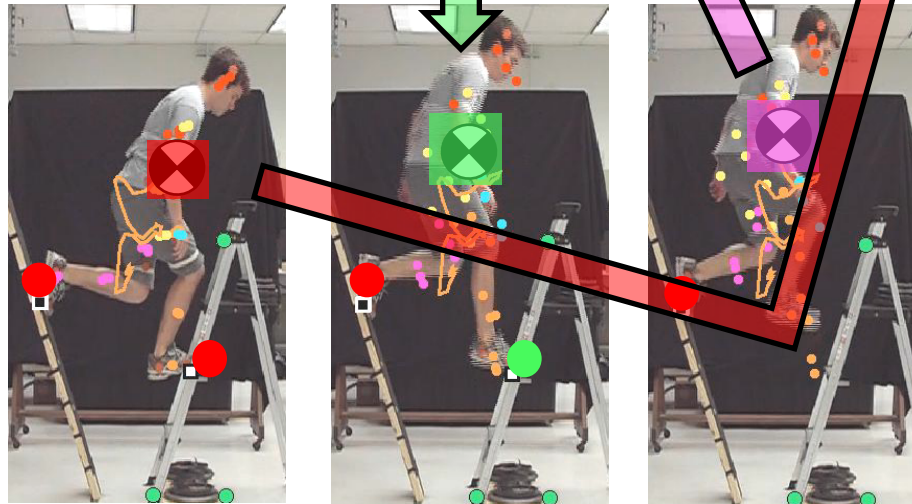
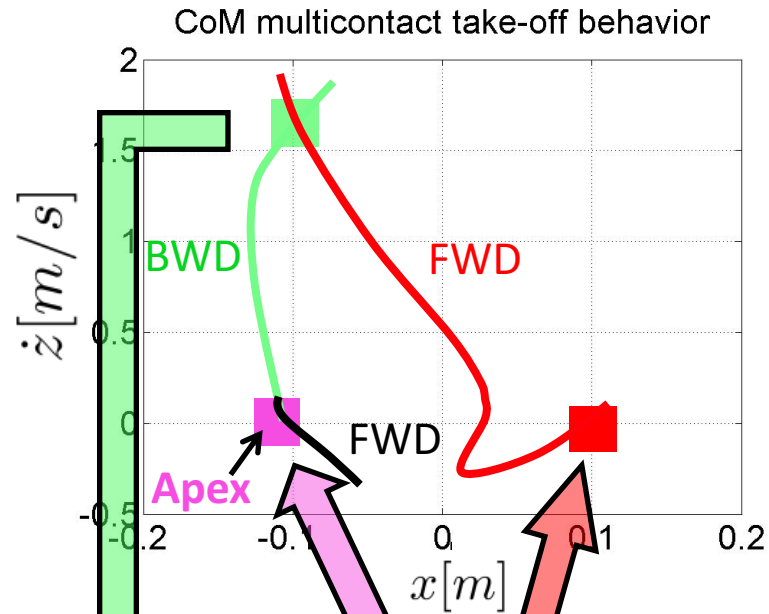
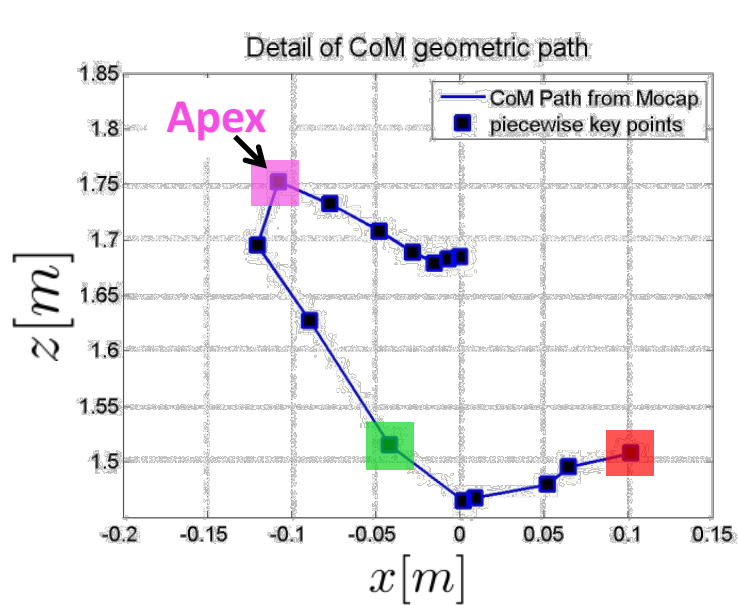


# Motion planning

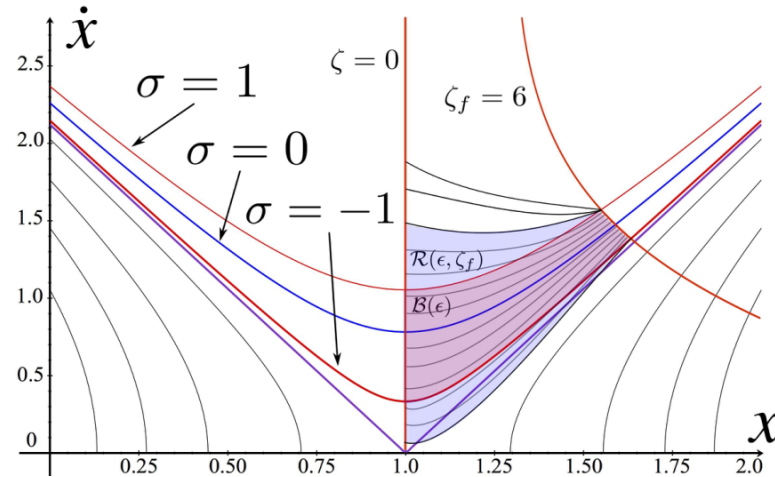


Like calculating the timing for bouncing in gymnastics... but simpler

# Example: Extreme Maneuver from Human Demonstration



# Tangent Manifold



$$\mathcal{M}_{\text{CoM}} = \left\{ \mathbf{x} \in \mathbb{R}^2 \mid \sigma(\mathbf{x}) = 0 \right\}$$

## Proposition: Phase-Space Tangent Manifold

Given desired PIP dynamics with  $(x_0, \dot{x}_0) = (x_{\text{foot}}, \dot{x}_{\text{apex}})$  and  $x_{\text{foot}}$ , the phase space tangent manifold is

$$\sigma = \frac{\dot{x}_{\text{apex}}^2}{\omega^2} \cdot \left( \dot{x}^2 - \dot{x}_{\text{apex}}^2 - \omega^2 (x - x_{\text{foot}})^2 \right)$$

where  $\sigma = 0$  is equivalent to the nominal manifold.



# Optimal Control

## Continuous Control: Dynamic Programming

$$\min_{\mathbf{u}_x^c} \mathcal{V}_N + \sum_{n=0}^{N-1} \eta^n \mathcal{L}_n$$

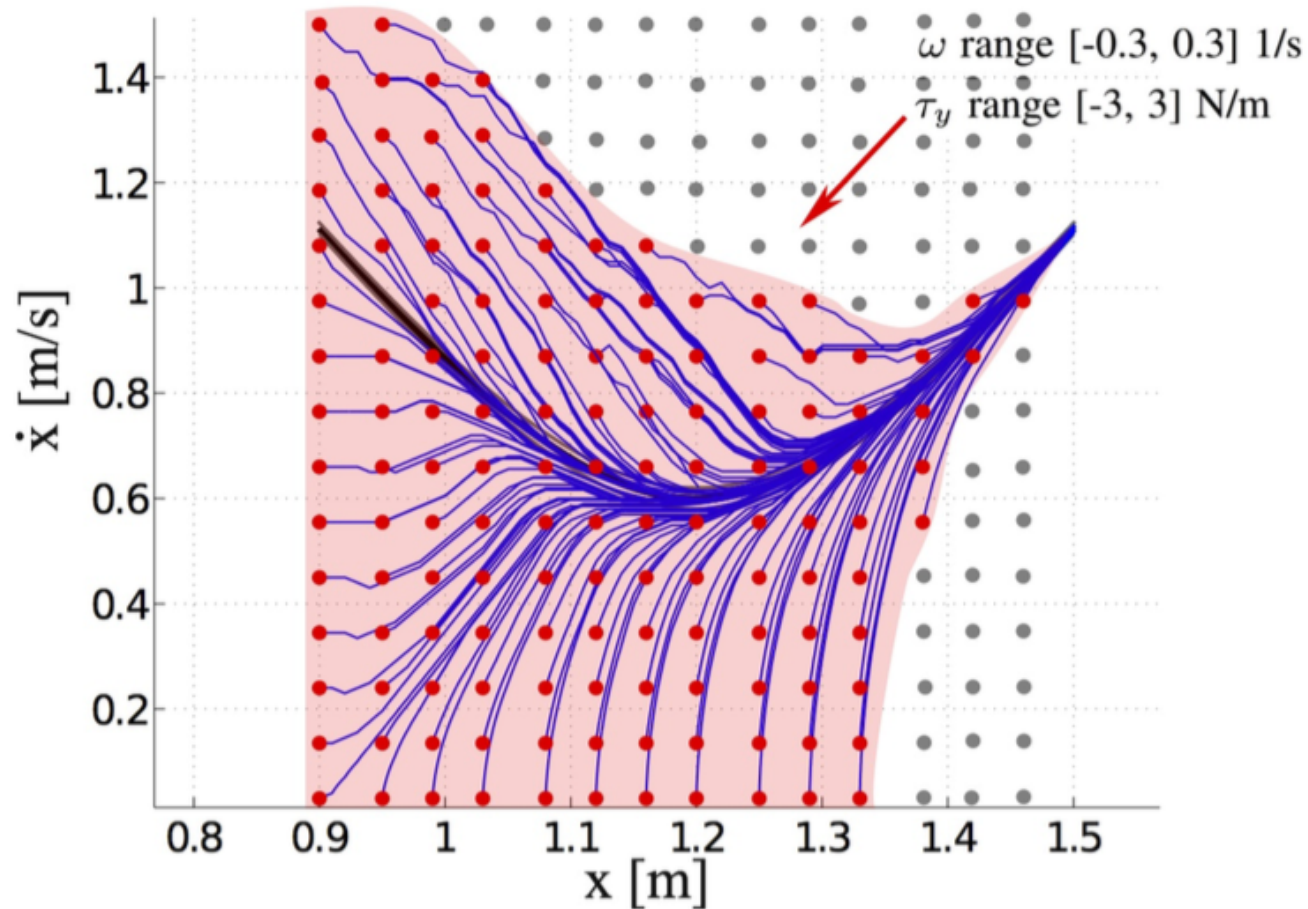
$$\text{subject to : } \dot{\mathbf{x}} = \mathcal{F}_x(q, \mathbf{x}, \mathbf{u}_x^c),$$

$$\omega \in [\omega^{\min}, \omega^{\max}],$$

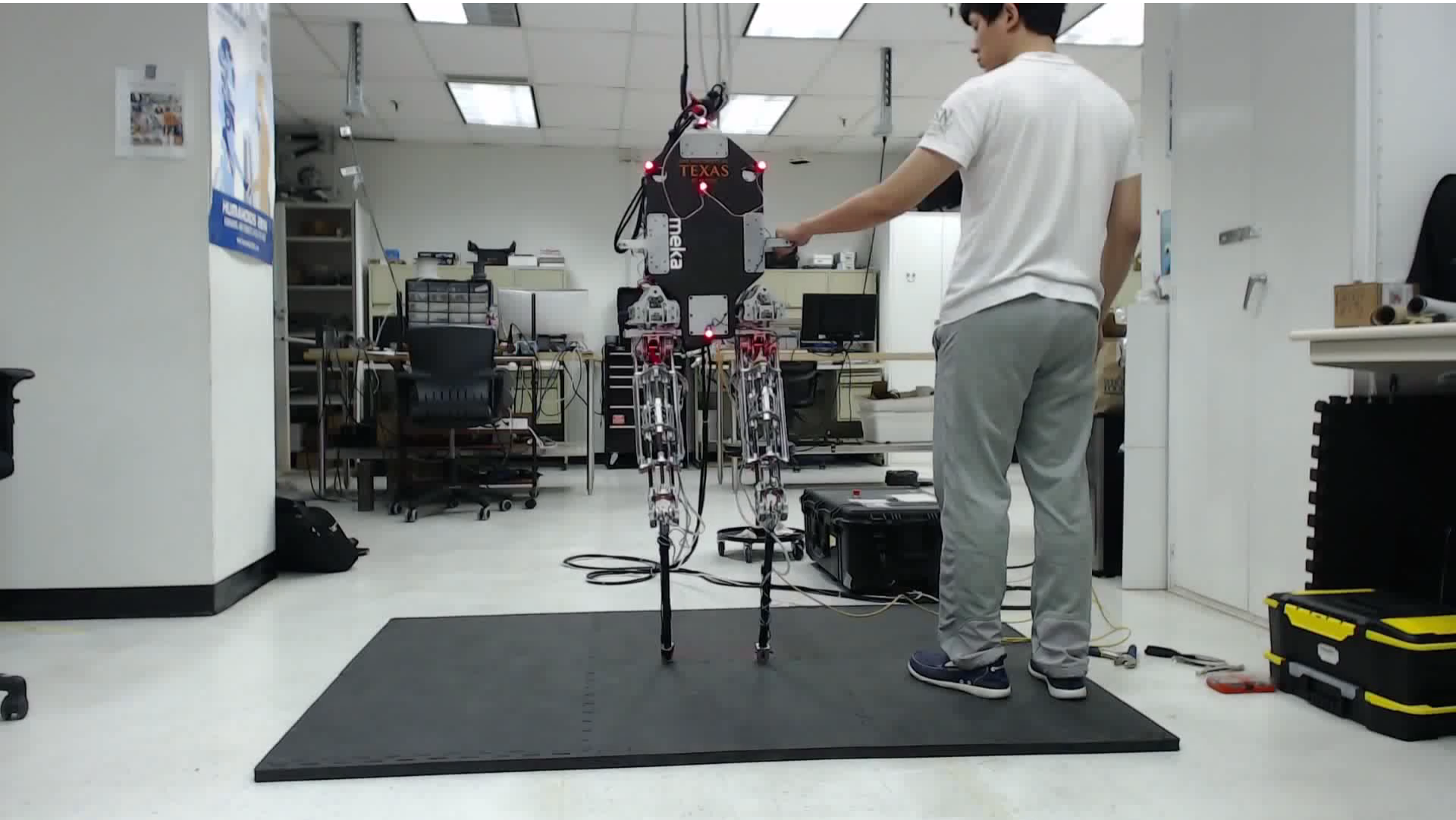
$$\tau_y \in [\tau_y^{\min}, \tau_y^{\max}]$$

$$\mathcal{L}_n = \int_{\zeta_n}^{\zeta_{n+1}} [\beta \sigma^2 + \Gamma_1 \tau_y^2 + \Gamma_2 (\omega - \omega^{\text{ref}})^2] d\zeta,$$

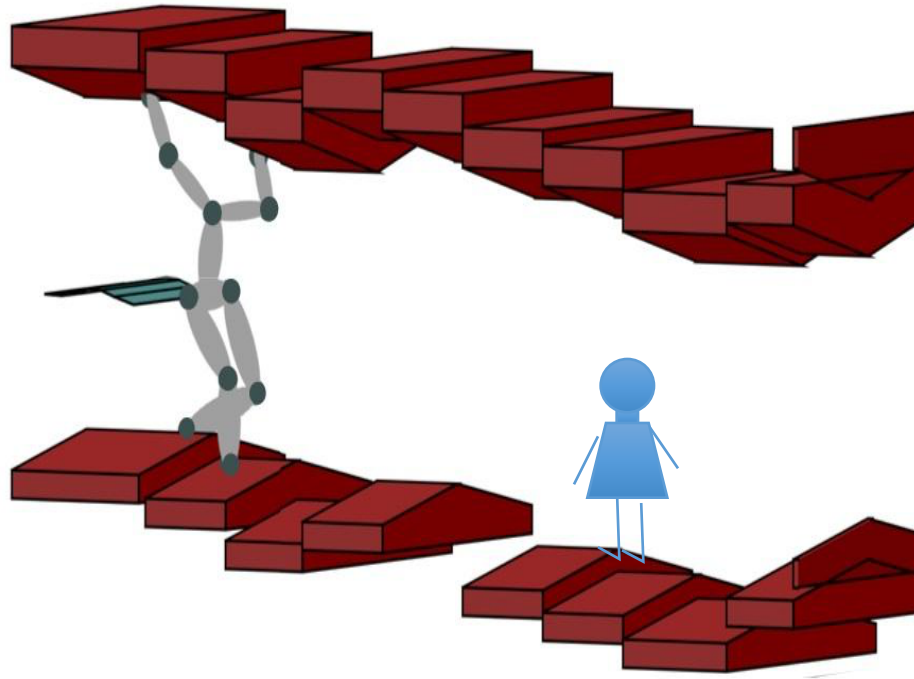
# Estimation of Recoverability Bundle



# Unsupported Dynamic Balancing

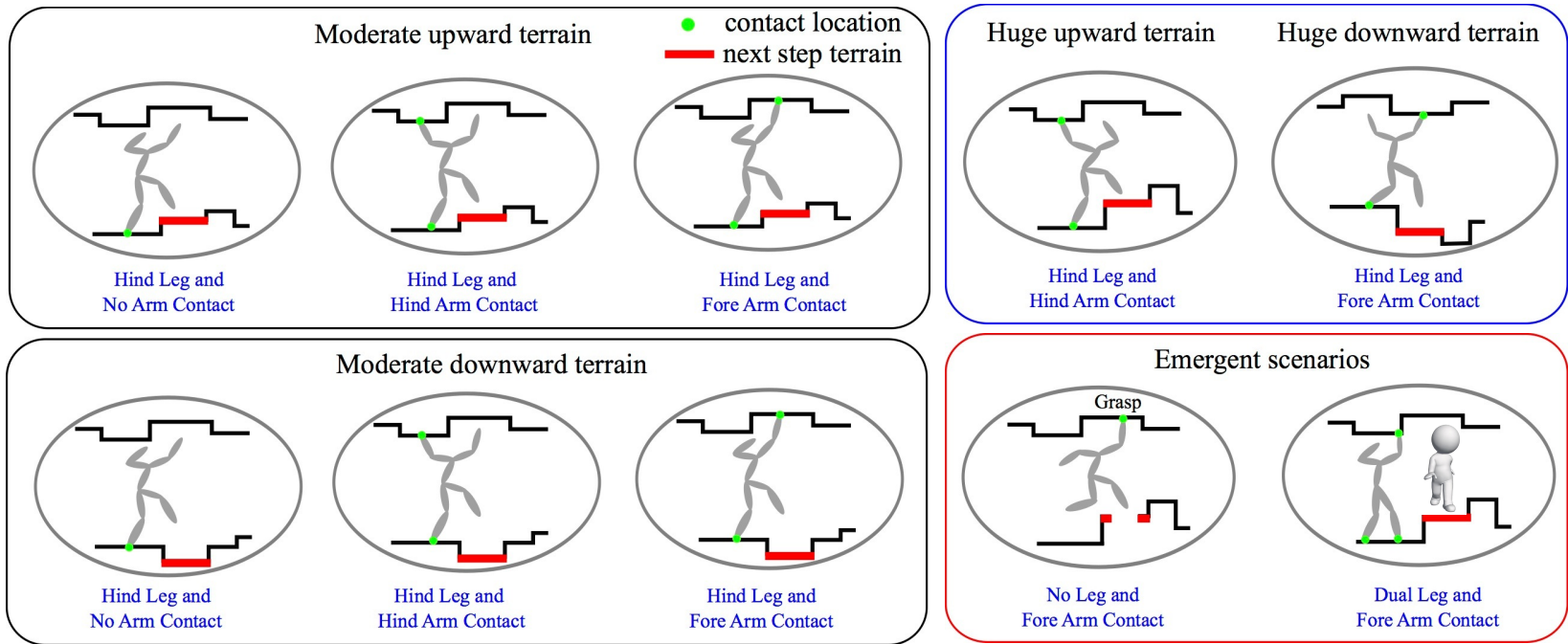


# Planner Synthesis

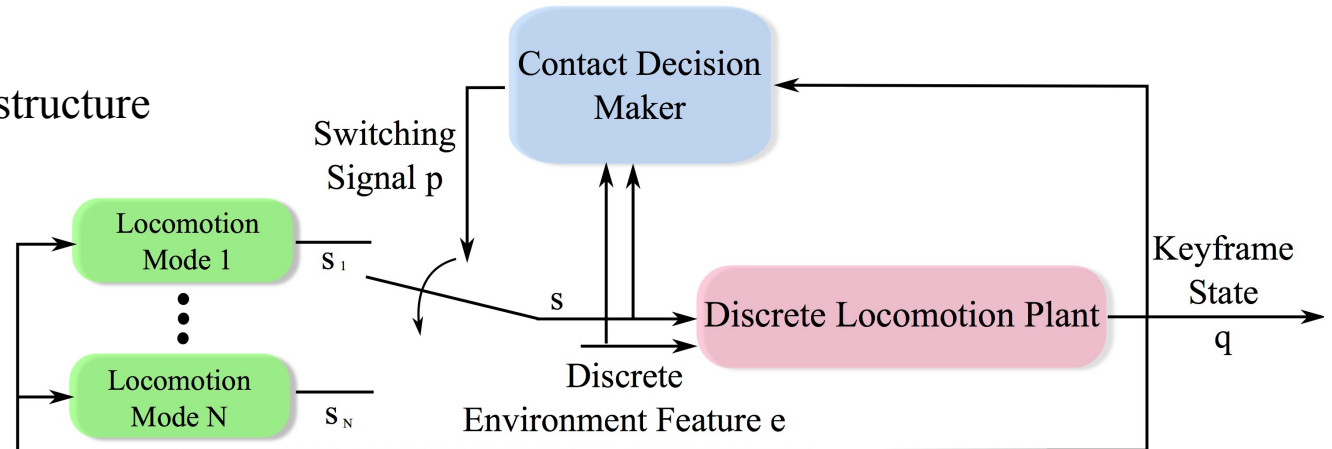


- *Traverse unstructured environments dynamically by using **all limbs**.*
- *React to diverse **dynamic events** by making sequential switching decisions.*
- *Satisfy all the required specifications in a **provably-correct manner**.*

# Contact Decisions for Constrained Environments



- Logic based planner structure





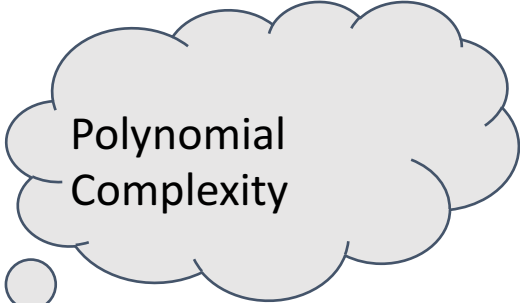
# Temporal Logic For Locomotion

An open finite transition system is a tuple

$$\mathcal{TS} = (\mathcal{Q}, \mathcal{P}, \mathcal{A}_{uc}, \mathcal{A}_c, \mathcal{T}, \mathcal{I}, AP, \mathcal{L})$$

Generalized Reactivity [1] formalism for tractability

$$\varphi_v = \varphi_{\text{init}}^v \bigwedge_{i \in I_{\text{safety}}} \square \varphi_{\text{trans},i}^v \bigwedge_{i \in I_{\text{goal}}} \square \diamond \varphi_{\text{goal},i}^v$$



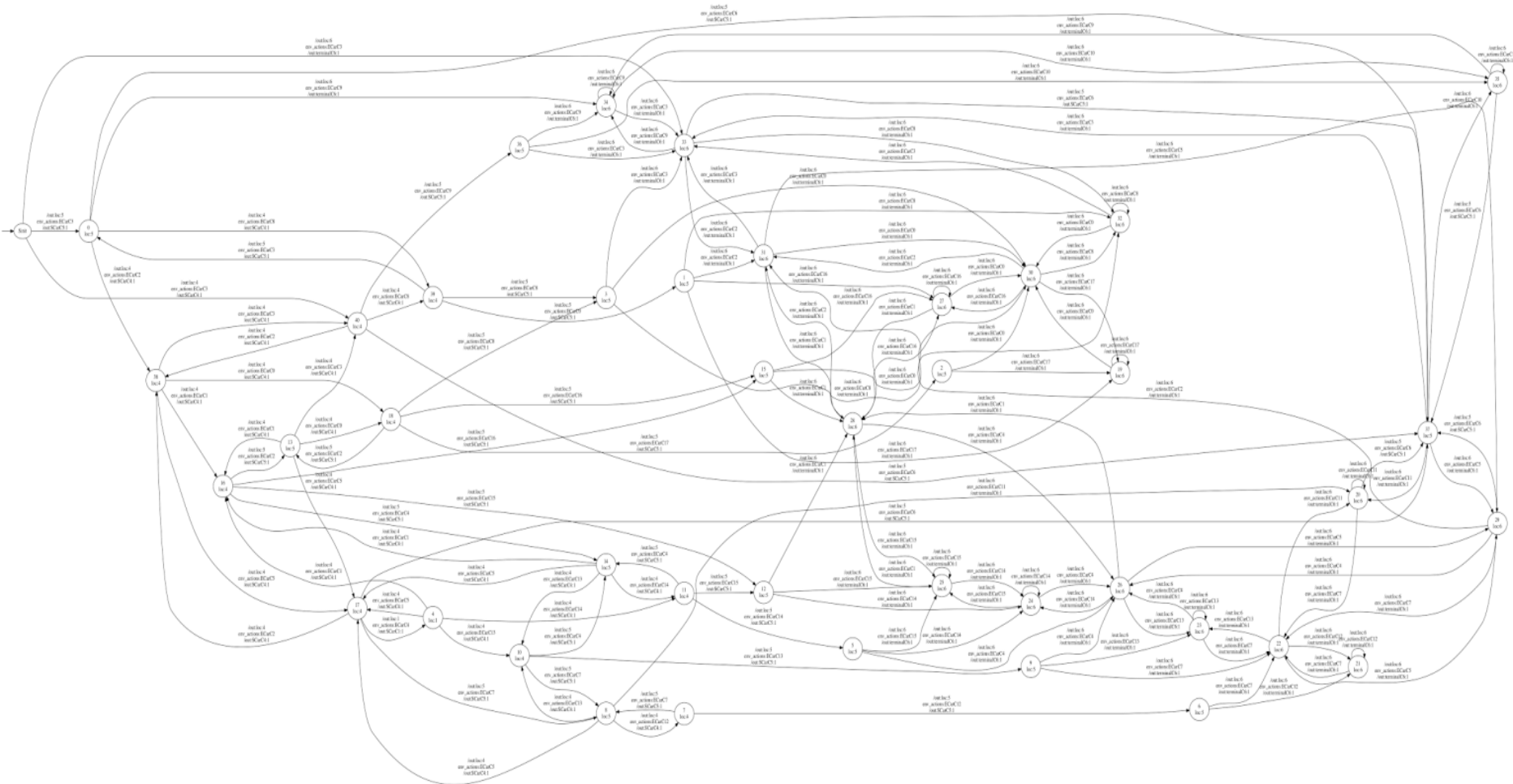
Polynomial  
Complexity

Final goal of the planner:

$$\varphi := ((\varphi_q \wedge \varphi_e) \Rightarrow \varphi_s)$$

**Discrete Contact Planner Switching Synthesis:** Given a transition system  $\mathcal{TS}$  and a LTL specification  $\varphi$ , this study synthesizes a contact planner switching strategy  $\gamma$  that generates only correct executions  $(q, p)$ , i.e.,  $(q, p) \models \varphi$ .

Manually creating an automaton would be challenging...



# Integrated Task and Motion Locomotion Planner



**E**

E

N

**N**

E

E

D

N

N

E

E

**D**

N

N

D